

Betatron functions

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- General solutions of Hill's equations
 - Floquet theory
- Betatron functions
- Transfer matrices revisited
 - General and periodic cell
- General transport of betatron functions
 - Drift
 - Beam waist
- Normalized coordinates

Solution of Betatron equations



- Symmetries of beam transport $x'' + K_x(s) x = 0$
- Betatron equations are linear with $y'' + K_y(s) y = 0$
periodic coefficients $K_x(s) = K_x(s + C)$, $K_y(s) = K_y(s + C)$

- **Floquet theorem** states that the solutions are $u(s) = Aw(s) \cos(\psi(s) + \psi_0)$

where $w(s)$, $\psi(s)$ are periodic with the same period

$$w(s) = w(s + C), \quad \psi(s) = \psi(s + C)$$

- Note that solutions resemble the one of harmonic oscillator

$$u(s) = A \cos(\psi(s) + \psi_0)$$

- Substitute solution in Betatron equations

$$u'' + K(s) u = \underbrace{A(2w'\psi' + w\psi'')}_0 \sin(\psi + \psi_0) + \underbrace{A(w'' - w\psi'^2 + Kw)}_0 \cos(\psi + \psi_0) = 0$$

- By multiplying with w the coefficient of **sin**
$$2w'w\psi' + w^2\psi'' = (w^2\psi')' = 0$$

- Integrate to get
$$\psi = \int \frac{ds}{w^2(s)}$$

- Replace ψ' in the coefficient of **cos** and obtain

$$w^3(w'' + K_x w) = 1$$

- Define the **Betatron** or **twiss** or **lattice functions** (Courant-Snyder parameters)

$$\begin{aligned}\beta(s) &\equiv w^2(s) \\ \alpha(s) &\equiv -\frac{1}{2} \frac{d\beta(s)}{ds} \\ \gamma(s) &\equiv \frac{1 + \alpha^2(s)}{\beta(s)}\end{aligned}$$

- The on-momentum linear betatron motion of a particle is described by

$$u(s) = \sqrt{\epsilon\beta(s)} \cos(\psi(s) + \psi_0)$$

with α , β , γ the twiss functions $\alpha(s) = -\frac{\beta(s)'}{2}$, $\gamma = \frac{1 + \alpha(s)^2}{\beta(s)}$

ψ the **betatron phase** $\psi(s) = \int \frac{ds}{\beta(s)}$

and the **beta function** β is defined by the **envelope equation**

$$2\beta\beta'' - \beta'^2 + 4\beta^2 K = 4$$

- By differentiation, we have that the **angle** is

$$u'(s) = \sqrt{\frac{\epsilon}{\beta(s)}} (\sin(\psi(s) + \psi_0) + \alpha(s) \cos(\psi(s) + \psi_0))$$

Courant-Snyder invariant



- Eliminating the angles by the position and slope we define the **Courant-Snyder invariant**

$$\gamma u^2 + 2\alpha u u' + \beta u'^2 = \epsilon$$

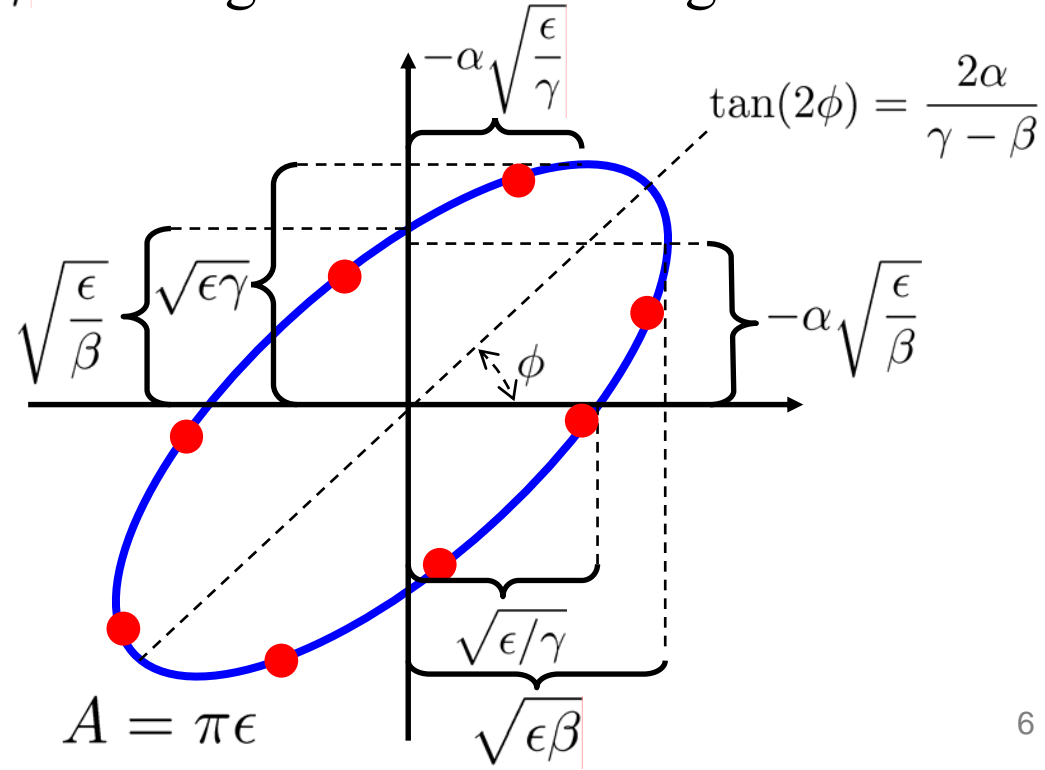
- This is an ellipse in phase space with area $\pi\epsilon$
- The twiss functions α , β , γ have a geometric meaning

- The beam envelope is

$$E(s) = \sqrt{\epsilon\beta(s)}$$

- The beam divergence

$$A(s) = \sqrt{\epsilon\gamma(s)}$$



- From equation for position and angle we have

$$\cos(\psi(s) + \psi_0) = \frac{u}{\sqrt{\epsilon\beta(s)}}, \quad \sin(\psi(s) + \psi_0) = \sqrt{\frac{\beta(s)}{\epsilon}}u' + \frac{\alpha(s)}{\sqrt{\epsilon\beta(s)}}u$$

- Expand the trigonometric formulas and set $\psi(0)=0$ to get the transfer matrix from location 0 to s

$$\begin{pmatrix} u(s) \\ u'(s) \end{pmatrix} = \mathcal{M}_{0 \rightarrow s} \begin{pmatrix} u_0 \\ u'_0 \end{pmatrix}$$

with

$$\mathcal{M}_{0 \rightarrow s} = \begin{pmatrix} \sqrt{\frac{\beta(s)}{\beta_0}} (\cos \Delta\psi + \alpha_0 \sin \Delta\psi) & \sqrt{\beta(s)\beta_0} \sin \Delta\psi \\ \frac{(a_0 - a(s)) \cos \Delta\psi - (1 + \alpha_0 \alpha(s)) \sin \Delta\psi}{\sqrt{\beta(s)\beta_0}} & \sqrt{\frac{\beta_0}{\beta(s)}} (\cos \Delta\psi - \alpha_0 \sin \Delta\psi) \end{pmatrix}$$

and $\Delta\psi = \int_0^s \frac{ds}{\beta(s)}$ the **phase advance**

- Consider a periodic cell of length C
- The optics functions are $\beta_0 = \beta(C) = \beta$, $\alpha_0 = \alpha(C) = \alpha$

and the phase advance
$$\mu = \int_0^C \frac{ds}{\beta(s)}$$

- The transfer matrix is

$$\mathcal{M}_C = \begin{pmatrix} \cos \mu + \alpha \sin \mu & \beta \sin \mu \\ -\gamma \sin \mu & \cos \mu - \alpha \sin \mu \end{pmatrix}$$

- The cell matrix can be also written as

$$\mathcal{M}_C = \mathcal{I} \cos \mu + \mathcal{J} \sin \mu$$

with $\mathcal{I} = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix}$ and the **Twiss matrix**

$$\mathcal{J} = \begin{pmatrix} \alpha & \beta \\ -\gamma & -\alpha \end{pmatrix}$$

- From the periodic transport matrix $\text{Trace}(\mathcal{M}_C) = 2 \cos \mu$ and the following stability criterion

$$|\text{Trace}(\mathcal{M}_C)| < 2$$

- In a ring, the **tune** is defined from the 1-turn phase advance

$$Q = \frac{1}{2\pi} \oint \frac{ds}{\beta(s)}$$

i.e. number betatron oscillations per turn

- From a general transfer matrix for a cell $\mathcal{M}_C = \begin{pmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{pmatrix}$ we get

$$\cos \mu = \frac{1}{2}(m_{11} + m_{22}), \quad \beta = \frac{m_{12}}{\sin \mu}, \quad \alpha = \frac{m_{11} - m_{22}}{2 \sin \mu}, \quad \gamma = -\frac{m_{21}}{\sin \mu}$$

- For a general matrix between position 1 and 2

$$\mathcal{M}_{s_1 \rightarrow s_2} = \begin{pmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{pmatrix} \text{ and the inverse } \mathcal{M}_{s_2 \rightarrow s_1} = \begin{pmatrix} m_{22} & -m_{12} \\ -m_{21} & m_{11} \end{pmatrix}$$

- Equating the invariant at the two locations

$$\epsilon = \gamma_{s_2} u_{s_2}^2 + 2\alpha_{s_2} u_{s_2} u'_{s_2} + \beta_{s_2} u'_{s_2}{}^2 = \gamma_{s_1} u_{s_1}^2 + 2\alpha_{s_1} u_{s_1} u'_{s_1} + \beta_{s_1} u'_{s_1}{}^2$$

and eliminating the transverse positions and angles

$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_{s_2} = \begin{pmatrix} m_{11}^2 & -2m_{11}m_{12} & m_{12}^2 \\ -m_{11}m_{21} & m_{11}m_{22} + m_{12}m_{21} & -m_{22}m_{12} \\ m_{21}^2 & 2m_{22}m_{21} & m_{22}^2 \end{pmatrix} \begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_{s_1}$$

Example I: Drift



- Consider a drift with length s

- The transfer matrix is $\mathcal{M}_{\text{drift}} = \begin{pmatrix} 1 & s \\ 0 & 1 \end{pmatrix}$

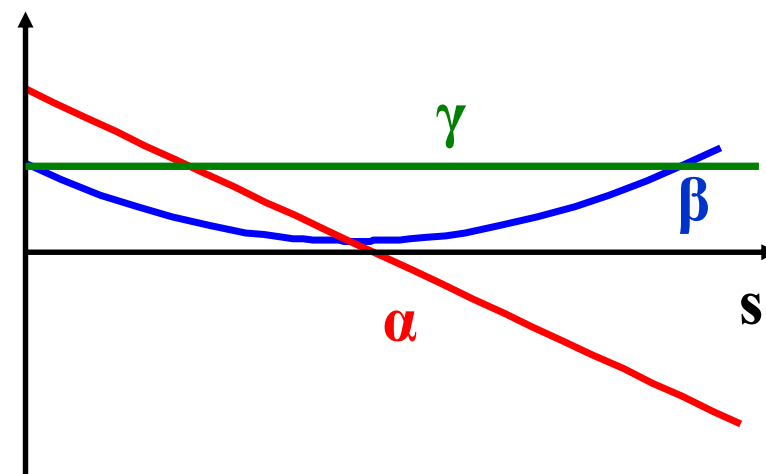
- The betatron transport matrix is $\begin{pmatrix} 1 & -2s & s^2 \\ 0 & 1 & -s \\ 0 & 0 & 1 \end{pmatrix}$

from which

$$\beta(s) = \beta_0 - 2s\alpha_0 + s^2\gamma_0$$

$$\alpha(s) = \alpha_0 - s\gamma_0$$

$$\gamma(s) = \gamma_0$$



- Consider the beta matrix $\mathcal{B} = \begin{pmatrix} \beta & -\alpha \\ -\alpha & \gamma \end{pmatrix}$ the matrix

$$\mathcal{M}_{1 \rightarrow 2} = \begin{pmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{pmatrix} \text{ and its transpose } \mathcal{M}_{1 \rightarrow 2}^T = \begin{pmatrix} m_{11} & m_{21} \\ m_{12} & m_{22} \end{pmatrix}$$

- It can be shown that

$$\mathcal{B}_2 = \mathcal{M}_{1 \rightarrow 2} \cdot \mathcal{B}_1 \cdot \mathcal{M}_{1 \rightarrow 2}^T$$

- Application in the case of the drift

$$\mathcal{B} = \mathcal{M}_{\text{drift}} \cdot \mathcal{B}_0 \cdot \mathcal{M}_{\text{drift}}^T = \begin{pmatrix} 1 & s \\ 0 & 1 \end{pmatrix} \begin{pmatrix} \beta_0 & -\alpha_0 \\ -\alpha_0 & \gamma_0 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ s & 1 \end{pmatrix}$$

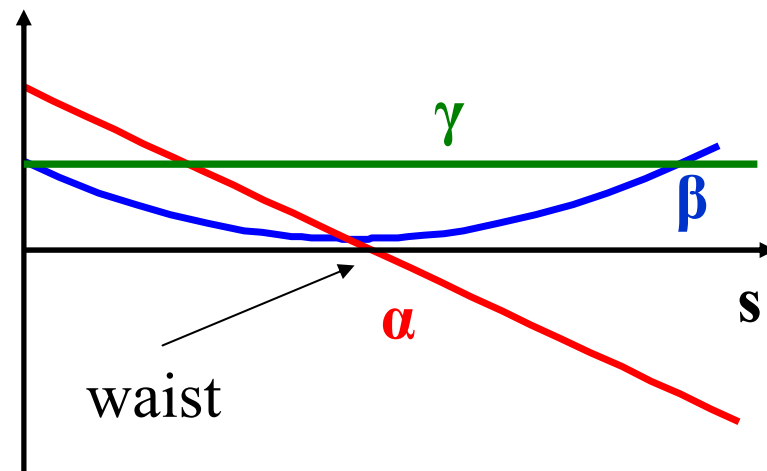
and

$$\mathcal{B} = \begin{pmatrix} \beta_0 - 2s\alpha_0 + s^2\gamma_0 & -\alpha_0 + s\gamma_0 \\ -\alpha_0 + s\gamma_0 & \gamma_0 \end{pmatrix}$$

Example II: Beam waist

- For beam waist $\alpha=0$ and occurs at $s = \alpha_0/\gamma_0$
- Beta function grows quadratically and is minimum in waist

$$\beta(s) = \beta_0 + \frac{s^2}{\beta_0}$$



- The beta at the waste for having beta minimum $\left. \frac{d\beta(s)}{d\beta_0} = 0 \right|$

at the entrance and exit of a drift with length \mathbf{L} is $\beta_0 = \frac{s}{2}$

- The phase advance of a drift is $\mu = \int_0^{L/2} \frac{ds}{\beta(s)} = \arctan\left(\frac{L}{2\beta_0}\right)$

which is $\pi/2$ when $\beta_0 \rightarrow \infty$. Thus, for a drift

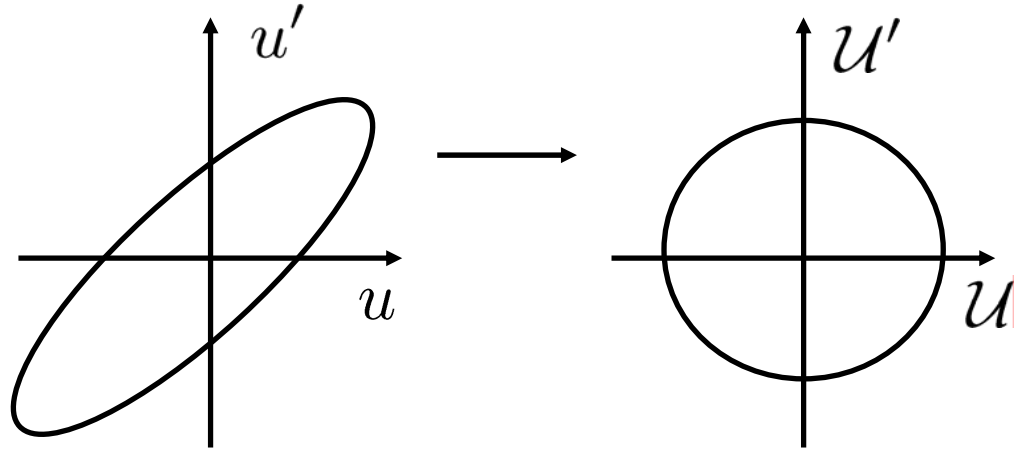
$$\mu \leq \pi$$

Normalized coordinates

- Introduce new variables
- In matrix form

$$u = \frac{u}{\sqrt{\beta}}, \quad u' = \frac{d\mathcal{U}}{d\phi} = \frac{\alpha}{\sqrt{\beta}}u + \sqrt{\beta}u', \quad \phi = \frac{\psi}{\nu}$$

$$\begin{pmatrix} \mathcal{U} \\ \mathcal{U}' \end{pmatrix} = \begin{pmatrix} \frac{1}{\sqrt{\beta}} & 0 \\ \frac{\alpha}{\sqrt{\beta}} & \sqrt{\beta} \end{pmatrix} \begin{pmatrix} u \\ u' \end{pmatrix}$$



- **Floquet transformation** transforms phase space in circles
- System becomes harmonic oscillator with frequency ν

$$\begin{pmatrix} \mathcal{U} \\ \mathcal{U}' \end{pmatrix} = \sqrt{\epsilon} \begin{pmatrix} \cos(\nu\phi) \\ -\sin(\nu\phi) \end{pmatrix}$$